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27NOV98 E407539-1 D00254
P01/7700 0.00 - 9825986.4

Request for grant of a patent

The Patent Office
Cardiff Road
Newport
Gwent NP9 1RH

1. Your Reference — **32/63132 GB**

2. Patent Application Number — **9825986.4** — 27 NOV 1998

3. Full name, address and postcode of the or of each applicant (*underline all surnames*)

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Patents ADP number (*if known*) 40984700 3

If the applicant is a corporate body, give the country/state of its incorporation — Country: **GERMANY** State:

4. Title of the invention — **IMPROVEMENTS IN OR RELATING TO REFRACTORY PRODUCTS**

5. Name of Agent — **FITZPATRICKS**

"Address for Service" in the United Kingdom to which all correspondence should be sent

4 WEST REGENT STREET
GLASGOW
G2 1RS

Patents ADP number — **00000695002**

6. Priority Details

Country	Priority Application Number	Date of filing
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7. If this application is divided or otherwise derived from an earlier UK application give details

Number of earlier application	Date of filing
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Patents f rm 1/77

8. Is a statement of inventorship and or right to grant of a patent required in support of this request?:

YES

9. Enter the number of sheets for any of the following items you are filing with the form.

Continuation Sheet for this form	---
Description	8
Claims	---
Abstract	---
Drawings	1 +1

10. If you are also filing any of the following state how many against each item.

Priority documents	---
Translations of priority documents	---
Statement of inventorship and right to grant of a Patent (*Patents Form 7/77*)	---
Request for Preliminary examination and search (*Patents form 9/77*)	----
Request for Substantive Examination (*Patents Form 10/77*)	---

11. I/We request the grant of a patent on the basis of this application

Signature ________ Date: **27 November 1998**

FITZPATRICKS

12. Name and daytime telephone number of person to contact in the United Kingdom

Eric Ede

0141 306 9000

Improv m nts in or r lating t refractory products

This invention relates to improvements in or relating to refractory products and, more particularly, to improvements in refractory products used in the handling of molten metals to increase reliability under high temperature operating conditions.

Metal teeming, and in particular the casting of steel usually begins with the metal being melted in a vessel e.g. a ladle or tundish. Refractory devices are required, amongst other things, for the regulation of the flow of the molten metal exiting from a nozzle mounted in the bottom of the vessel. In the casting of steel, this is typically applied through an opening in the base of the vessel via nozzles and shrouds into a water-cooled mould. Refractory devices such as sub-entry shrouds and pouring nozzles are often at least partly submerged for long periods of time in the molten metal during the metal teeming process and are therefore subject to high temperatures and stresses during the effective lifetime of the device.

In a typical teeming process, metal is melted in a furnace, transferred first to a ladle and then to a tundish from which it flows in a controlled manner into a cooled mould. A flow control valve is provided in the tundish comprising a flow control stopper rod selectively engageable with an outlet nozzle seat. The stopper would normally be raised off the seat by a certain amount to achieve a particular rate of flow of molten metal through the valve to ultimately cast a product in a mould.

The teeming apparatus would usually include a pouring nozzle or a shroud located beneath the flow control valve either of which may be immersed in melt as the casting operation proceeds.

In an exchange nozzle casting mechanism, the pouring nozzle or shroud is supported beneath a sliding plate which is used for sealing off

the flow of molten metal above the pouring nozzle or shroud to allow the pouring nozzle or shroud to be changed during the teeming process.

EP-A-0 346 378 describes the development of a monotube configuration and compares that to a two part plate and tube assembly generally known and used within an exchange nozzle casting mechanism as described above. The pouring tube element combines a body of high thermal shock resistance and corrosion resistance with a sliding plate surface able to form a tight closure against the stationary components of the mechanism. The sliding plate surface also incorporates a hard edge to permit cutting through any metal skin which may form during the casting operation and which may restrict free movement of the exchange monotube during the replacement procedure.

An important advantage of the monotube configuration over the original two part plate and tube or cast plate configuration was the elimination of generally horizontal joints connecting the internal casting bore of the tube with the external atmosphere, thereby eliminating the risk of air ingress or metal leakage across this joint region.

As casting conditions have become more severe and service life requirements of refractory products increased, new demands have been placed on the monotube elements of an exchange nozzle casting mechanism.

In meeting these demands alternative compositions for the pouring tube element have been developed making it possible to maintain the plate surface and cutting edge configuration whilst providing improved corrosion and erosion resistance. These improved materials for the pouring tube element of a monotube do however exhibit different thermo-mechanical properties from the original materials as shown in the following table.

MONOTUBE POURING TUBE ELEMENT COMPOSITIONS

CONVENTIONAL		HIGH CORROSION RESISTANCE
40	Al_2O_3%	64
18	SiO_2 %	6
28	C%	24
8	ZrO_2%	6
4	SiC%	-
2.38	Bulk density g/ml	2.6
0.35	Thermal Expansion% 0-1000	0.52

In operation, it has been shown that whilst the overall criteria for performance improvement has been met there is an increased risk that thermo mechanical stresses arising at the outset of casting can cause an external micro-crack fracture at the section change between the head and body portions of the pouring tube. In many instances, this micro-crack fracture is contained by the inherent integrity of the ceramic body. This results in no operational problem, but in extreme cases it is possible for the external micro-crack fracture to propagate across the ceramic wall of the tube to the inner bore. This allows either air ingress or metal leakage, both of which cause termination of the cast and possible damage to the exchange nozzle casting mechanism.

Extensive computer simulation of the thermo-mechanical stresses arising during preheat and start up of casting has now identified the possibility of minimising the stresses leading to such micro-crack fractures and subsequent propagation by minimising the thermal gradient across the ceramic pouring element at this region of large cross section change and by providing external support below this section change.

Studies of the behaviour of the conventional metallic can and pouring tube element showed that the metallic can, essential to provide the accurate geometry required for a precise fit into the exchange nozzle

casting mechanism could also act to transfer heat from the pouring element into the cooled mechanical mechanism, thereby increasing the thermal gradient at this critical point. Additionally at the temperatures experienced during preheat prior to cast start up the lower region of the can would reach a temperature of approx. 900 C at which the relatively mild steel from which it is formed loses its rigidity and ceases to provide the desirable structural support below the section change.

An object of this invention is to obviate or mitigate the risks of exaggerated thermo mechanical stresses in the new generation of pouring tube elements, and this is found to be achievable by revising both the design of the pouring tube element and the manner in which it is contained within the can. It will be recalled that location of the refractory within the support can requires care to provide the correct geometrical configuration to allow effective operation of the exchange tube mechanism and maintain the principle of no direct horizontal connection from the bore to the exterior other than the machined sliding surface.

According to one aspect of the present invention there is provided a refractory device for use in the teeming of molten metal comprising a ceramic body having a ceramic pouring tube element and a support element, said support element being adapted to be received within a metallic can, and there is provided between said elements a shock-absorbing interface zone wherein there is provided a material the thermal properties of which are such that it is substantially solid at ambient temperatures but becomes deformable at the elevated temperatures experienced during metal teeming.

Thus, the interface zone provides continuity of mechanical support to the body portion when in the substantially solid (cool ambient temperature) condition to ensure structural integrity of the assembled refractory device, but deforms sufficiently to provide a buffer against sudden differential thermal stresses, thereby minimising the risks of

micro-crack fracture through the body portion due to thermo mechanical stresses during pre-heat and at the start of the casting operation.

Advantageously, the material selected for use in the interface zone is structurally solid at temperatures up to about 700 C and becomes deformable without any appreciable chemical degradation at temperatures above about 700 C.

Preferably, the interface zone comprises a refractory material such as a paste or bonding agent or additional structural refractory element exhibiting the aforesaid properties, and may be a glaze applied over at least one of the co-operating assembly surfaces of the pouring tube element and the support element.

The support element is normally fully encapsulated within the metallic can, and fits with and around the upper part of the pouring tube element by virtue of said support element having an internal profile corresponding sufficiently to the external profile of the pouring tube. Conveniently, the respective profiles are such as to provide corresponding interference fit surfaces or otherwise matching e.g. tapering surfaces to facilitate assembly, and in-fill or insertion of the required shock-absorbing interface zone material.

The support element may be pre-formed from a ceramic material of low thermal conductivity, or formed *in situ* by a suitable moulding operation of a type familiar to those in this art.

The refractory device may be otherwise finished as is known in the art to suit its intended purpose, e.g. with regard to provision of flat surfaces and outlet nozzles etc.

Embodiments of the invention will now be described with reference to the accompanying drawings in which:

Figure 1 is a cross-sectional view of a two-part plate and tube configuration in accordance with prior art;

Figure 2 is a cross-sectional view of a prior art monotube configuration;

Figure 3 is a cross-sectional view of a monotube configuration showing a stress micro-crack fracture of the type minimised by the present invention;

Figure 4 is a cross-sectional view of a refractory device according to one aspect of the present invention; and

Figure 5 is a cross-sectional view of a refractory device according to a second aspect of the present invention.

Referring now to the figures, there is shown in figures 1-3 cross-sectional views of prior art refractory devices including the two-part plate and tube assembly known generally in the prior art and the early monotube configuration discussed above.

Figure 4 is a cross-sectional view of a refractory product according to one aspect of the present invention. This shows a refractory pouring device having a ceramic pouring tube element **10** such as for example of a pouring nozzle or sub entry shroud. The pouring tube element is supported in a metallic can **11**, which maintains the desired geometrical configuration of the tube for mechanical integrity of the pouring mechanism. A low thermal conductivity ceramic element **12** is encapsulated within the metallic can, and fits with and around the upper part of the pouring tube element, by virtue of said ceramic element having an internal profile corresponding sufficiently to the external profile of the pouring tube. Here, a stepped shoulder, interference fit arrangement is illustrated.

The low thermal conductivity of the ceramic element reduces heat losses from the pouring tube during metal teeming thereby minimising the differential thermal stresses experienced by the pouring tube which could lead to propagation of stress micro-crack fractures.

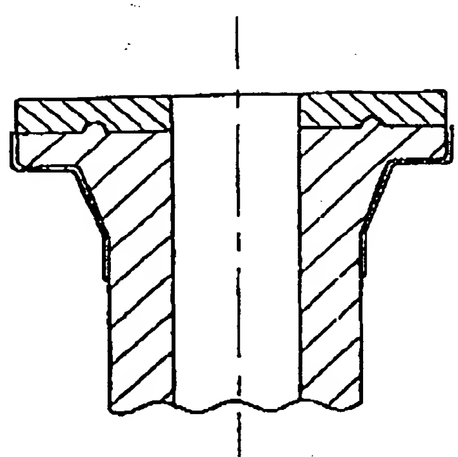
A shock absorbing interface zone **13** is formed between the low conductivity ceramic element 12 and the pouring tube element 10. The zone is formed in accordance with one aspect of the invention by a layer of refractory ceramic cement, the properties of which are chosen to provide optimum mechanical strength in temperatures below about 550 C to support the pouring tube during preheating operations and manipulation. The cement has a degree of malleability at elevated temperatures encountered during use of the pouring tube in the metal teeming process to absorb any residual differential stresses, which may be created during this process.

Figure 5 illustrates a further embodiment of the present invention wherein the pouring tube element **20** is coated with a surface layer **24** on its upper region. The surface coating may be a glaze, which provides low temperature rigidity and high temperature malleability. The coated tube is then encapsulated within the metallic can by a ceramic mass **22**, which provides mechanical support to the pouring tube during the teeming process. Furthermore, the ceramic element reduces heat losses from the pouring tube during metal teeming thereby minimising the differential thermal stresses experienced by the pouring tube which lead to propagation of stress micro-crack fractures.

In use of either of the refractory device described above, the pouring tube is mounted beneath the orifice of a vessel (not shown). Molten metal is poured through the pouring tube for example into a water-cooled mould (not shown). During the metal casting process, the external temperature of the pouring tube rises typically to between 700 C and 900 C. At temperatures up to about 700 C, the interface zone

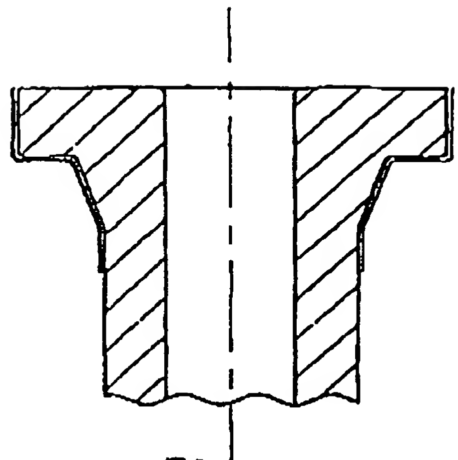
(13; 24) between the pouring tube element (10; 20) and the ceramic element (12; 22) encapsulated in the metallic can remains solid and provides structural continuity and additional mechanical support to the pouring tube. Thereby, structural integrity of the refractory device is provided for e.g. during handling for transport purposes, and initially during assembly into a pouring mechanism and pre-heat. At temperatures above about 700 C however, at which differential thermal stresses between the pouring tube and the support therefor in the metallic can would have previously possibly caused a stress micro-crack fracture of the pouring tube, the interface zone becomes deformable, thereby minimising differential thermal stresses experienced by the pouring tube in the region supported by the metallic can. Therefore, in this way the possibility of micro-crack fracture through the refractory device and failure thereof is obviated or mitigated. Thus, the present invention results in an improved refractory device that has better reliability and is less prone to damage from differential stress micro-crack fractures.

Fig 1.



PRIOR ART

Fig 2.



PRIOR ART

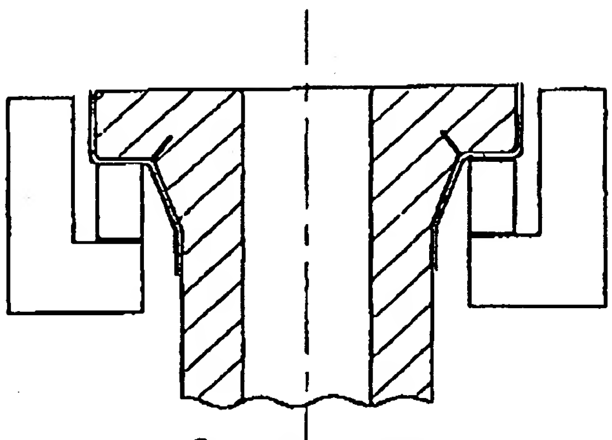


Fig 3.

PRIOR ART

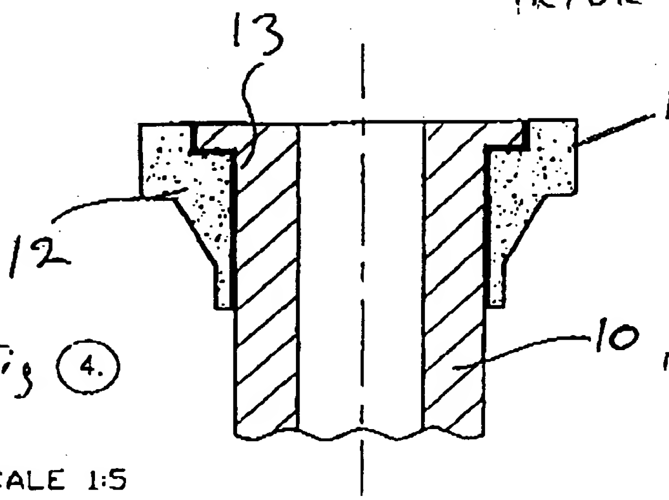


Fig 4.

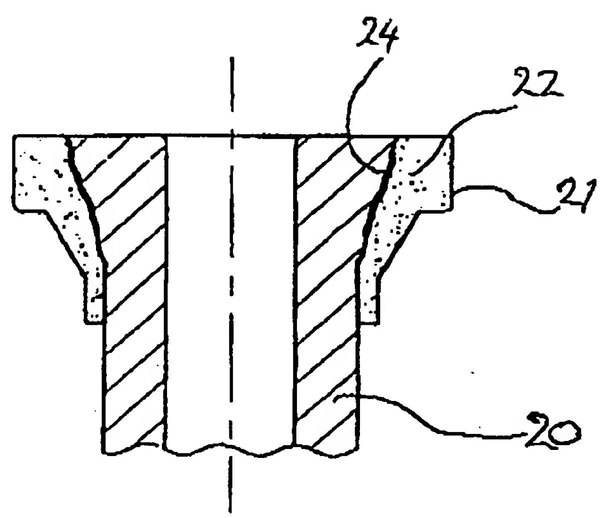


Fig 5.

SCALE 1:5